

PATENT ABSTRACTS OF JAPAN

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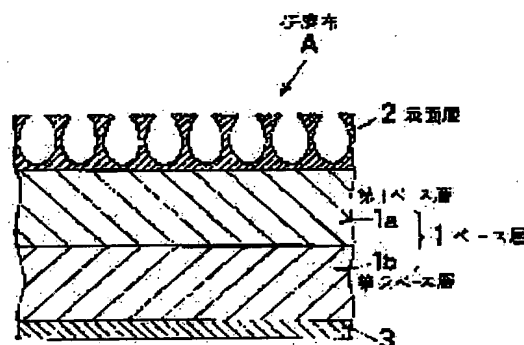
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(54) ABRASIVE CLOTH

(57)Abstract:

PURPOSE: To provide an abrasive cloth with which generation of deterioration of surface roughness, injury, or the like are not caused and roll-over of the end face can be restrained when a workpiece to be polished is polished.

CONSTITUTION: A target is an abrasive cloth in which a surface layer 2 for polishing is laminated on the surface of a base layer 1 made of nonwoven fabric. The base layer 1 is formed into double laminated construction constituted of a first base layer 1a positioned on the surface layer 2 side and a second base layer 1b positioned on the back of the first base layer 1a. Hardness of the first base layer 1a is prescribed to be over hardness 80° by the spring type hardness test model C indicated in JIS K6301, and hardness of the second base layer 1b is prescribed to be under hardness 80° by the same test.



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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Industrial Application] This invention relates to the abrasive cloth used for polish processing of an aluminum (that alloy is included) magnetic-disk substrate, the wafer for semi-conductors, an optic lens, the mask for wafers, a metal sample, etc.

[0002]

[Description of the Prior Art] The above polish processings of a ground workpiece are performed as follows, for example. That is, using the grinder which pasted up abrasive cloth on the vertical surface plate of a double-sided level-type grinder, a vertical surface plate is pressurized in 1 constant pressure, and the pressure welding of abrasive cloth and the ground workpiece is carried out. And after supplying a loose grain, rotation is given to a vertical surface plate and a ground workpiece, and the front face of a ground workpiece is ground by sliding abrasive cloth and a ground workpiece.

[0003] Covering formation of the surface layer for polish (52) of the porosity which becomes the front face of the base layer (51) which consists of nonwoven fabrics, such as polyester fiber, from polyurethane etc. is carried out in one, and the abrasive cloth used for polish processing which carried out [above-mentioned] instantiation has the structure with which the glue line (53) for adhesion to a surface plate (60) was further covered by the rear face of a base layer (51), as generally shown in drawing 4.

[0004]

[Problem(s) to be Solved by the Invention] By the way, recently, it follows on small [of a ground workpiece], and the request of highly-precise-izing, and the severe surface characteristic after processing is increasingly required also about polish processing.

[0005] However, if polish processing is performed using the conventional abrasive cloth, as shown in drawing 4 The result to which the compression set of the part in contact with the ground workpiece (70) of abrasive cloth (50) is greatly carried out by resiliency, The level difference for a part for a variant part (54) and a non-variant part (55) becomes large, and it will be in the condition that covered the edge section of a ground workpiece (70) which is located in the boundary for a part for a variant part (54), and a non-variant part (55) for this reason in the shape of a curve, and the front face of abrasive cloth contacted. When polish processing was performed in such the condition, since big thrust joined the edge section of a ground workpiece (70) from across, there was a problem that the edge section was ground the letter of an inclination thru/or in the shape of radii, and produced the so-called end-face sagging (71).

[0006] For this reason, the attempt which stops the compression deformation of abrasive cloth as much as possible, has it, and controls end-face sagging by infiltrating a curing agent into the surface layer (52) of abrasive cloth (50) is also made.

[0007] However, by this approach, when extent of hardening processing was too intense, it was what derives the new problem that it cannot become the cause of causing the fall of the surface roughness of a ground workpiece (70), or making a front face producing a blemish, a scratch, etc., and the good surface state after polish processing cannot be acquired. For this reason, there is a limitation in hardening processing of a surface layer, and certain and sufficient control of end-face sagging was not able to be aimed at.

[0008] Moreover, although to make thickness of a base layer (51) thin, to stop and have the

resiliency of the whole abrasive cloth and to lessen compression deformation was also tried. When thickness of a base layer (51) was made thin, the effect by the thickness of a glue line (53) and the effect by the blemish of a surface plate (60) and projection were what derives the problem of it being succeeded by the surface layer (2) and having big effect on the surface characteristic after polish processing too.

[0009] This invention is made in view of this technological background, and it aims at offer of the abrasive cloth which can control end-face sagging, without causing generating of the fall of the surface roughness at the time of polish processing, a blemish, etc. about a ground workpiece.

[0010]

[Means for Solving the Problem] In the abrasive cloth with which the laminating of the surface layer for polish (2) was carried out to the front face of the base layer (1) which consists of a nonwoven fabric when this invention was shown with reference to the sign of drawing 1, in order to attain the above-mentioned purpose. While said base layer (1) is formed in the double laminated structure by the 1st base layer (1a) located in a surface layer (2) side, and the 2nd base layer (1b) of the rear face. Said 1st base layer (1a) is specified to the degree of hardness of 80 degrees or more in the spring hardness test C form shown in JISK6301. Said 2nd base layer (1b) is JIS. Let abrasive cloth characterized by what is specified to the degree of hardness of less than 80 degrees in the spring hardness test C form shown in K6301, respectively be a summary.

[0011]

[Function] The 1st base layer (1a) which adjoins a surface layer (2) is JIS. Since it is specified to the degree of hardness of 80 degrees or more in the spring hardness test C form shown in K6301. The resiliency of the 1st base layer (1a), as a result the whole abrasive cloth is reduced, the compression deformation when carrying out a pressure welding to a ground workpiece at the time of polish processing becomes small, and the level difference for a part for a variant part and a non-variant part becomes small. For this reason, the thrust from the abrasive cloth given to the edge section of a ground workpiece located in the boundary for a part for the variant part of abrasive cloth and a non-variant part is mitigated, and end-face sagging is controlled as a result. On the other hand -- the 2nd base layer (1b) -- JIS since it is specified to the degree of hardness of less than 80 degrees in the spring hardness test C form shown in K6301, the effect of the surface plate parallelism by the fall of resiliency mitigates -- having -- the life-shortening of the piece skid of abrasive cloth, or abrasive cloth -- the abnormalities in parallelism of a ground workpiece are prevented further.

[0012]

[Example] Next, the example of this invention is explained.

[0013] Drawing 1 shows the abrasive cloth (A) concerning one example of this invention. In drawing 1, it is formed in porosity that the base layer which (1) becomes from the nonwoven fabric made from polyester fiber, and (2) should hold the loose grain with which it is the surface layer for polish made from polyurethane by which covering formation was carried out in [the front face of this base layer (1)] one, and this surface layer (2) is supplied on the occasion of polish processing. Moreover, the glue line (3) which consists of a double-sided tape is formed in this rear face, and it can paste up abrasive cloth (A) on a surface plate through this glue line (3) while priming of the rear face of a base layer (1) is carried out.

[0014] Moreover, by this invention, said base layer (1) is the 1st base layer (1a). While making double product layer structure with the 2nd base layer (1b). The 1st base layer (1a) which adjoins a surface layer (2) is JIS. It is specified to the degree of hardness of 80 degrees or more in the spring hardness test C form shown in K6301. The 2nd base layer (1b) on the rear face of the 1st base layer (1a) is JIS. It must have the degree of hardness specified to the degree of hardness of less than 80 degrees in the spring hardness test C form shown in K6301, respectively. In the spring hardness test C form specified to JISK6301. Although it is the determination-of-hardness trial which performs this test piece using C form of a spring hardness tester, using a thing (a less than 6mm thing putting and being 6mm or more if possible) with a thickness of 6mm or more as a principle and is the trial for measuring the hardness of vulcanized rubber essentially as a test piece. In this invention, this is applied correspondingly as a hardness test of the 1st and 2nd base layer (1a) (1b). The hardness of the 1st base layer (1a) is specified to the degree of hardness of 80 degrees or more in the above-mentioned trial here because it cannot fully aim at control of end-face sagging by the degree of

hardness of less than 80 degrees. That is, by the degree of hardness of less than 80 degrees, as a result of compression deformation's when the 1st base layer is too flexible and carries out a pressure welding's to a ground workpiece at the time of polish processing being too large, the level difference for a part for a variant part and a non-variant part becomes large. For this reason, it is because the big thrust from slant is given to the whole edge section of a ground workpiece located in the boundary for a part for the variant part of abrasive cloth, and a non-variant part and generating of end-face sagging cannot be controlled as a result. Conversely, it is because the difference of the deformation for a part for the compression variant part of abrasive cloth and a non-variant part can be lessened, the thrust from the abrasive cloth given to the edge section can be mitigated and generating of end-face sagging can be controlled as a result by making the 1st base layer (1a) into the degree of hardness of 80 degrees or more, if it says. The hardness of the 1st base layer (1a) is good to set this as the degree of hardness of 90 degrees or more in the above-mentioned trial especially preferably. [0015] Especially the means for specifying a base layer (1) to the degree of hardness of 80 degrees or more is not limited, forms a base layer with a hard nonwoven fabric, increases the consistency of a nonwoven fabric, infiltrates a curing agent into an elasticity base layer, or can mention the thing approach.

[0016] having *(ed) and having specified the hardness of the 1st base layer (1a) above -- the resiliency of the 1st base layer (1a), as a result the whole abrasive cloth (A) -- falling -- this sake -- the effect of surface plate parallelism -- winning popularity -- easy -- becoming -- the cause of the piece skid of abrasive cloth, and the life-shortening of abrasive cloth -- it becomes the cause of the abnormalities in parallelism of a ground workpiece further. Then, it is JIS about the hardness of the 2nd base layer (1b). By specifying to the degree of hardness of less than 80 degrees in the spring hardness test C form shown in K6301, a certain amount of resiliency is secured and the above-mentioned fault is prevented.

[0017] Incidentally, while setting to 0.5mm in 0.5mm in 1.0mm in thickness of the 1st base layer (1a), and thickness of the 2nd base layer (1b), and thickness of a surface layer (2) It is JIS only about the degree of hardness of the 1st base layer (1a) and the 2nd base layer (1b). The generating situation of end-face sagging was investigated using some kinds of abrasive cloth specified in the spring hardness test C form specified to K6301, respectively as shown in the following table. Moreover, the same trial was performed even if it used the conventional abrasive cloth whose base layer is 1 layer structure.

[0018] In addition, as shown in drawing 2 as a test piece, it is a diameter L1. : Diameter L2 except 95mm and the outside chamfer section (11) : 94.7mm, An aluminum magnetic-disk substrate (10) with a thickness of t:1.27mm is used. From the inside edge of the outside chamfer section (11) to the method L3 of inside : The sagging test section (12) was set up over the range of 4mm, and the difference of elevation H (shown in drawing 3) of the edge in this sagging test section (12) was measured as an amount of sagging. The result is shown in Table 1.

[0019]

[Table 1]

	第 1 ベース層硬度	第 2 ベース層硬度	ダレ量 (H) (μm)
従来例	な し	75°	0.3
比較例	75°	75°	0.25
実施例 1	80°	75°	0.15
実施例 2	90°	75°	0.08

[0020] As shown in the above-mentioned table 1, it could check that end-face sagging of a ground workpiece could be controlled sharply by specifying the degree of hardness of the 1st base layer (1a) and the 2nd base layer (1b) in this invention range.

[0021]

[Effect of the Invention] In the abrasive cloth with which the laminating of the surface layer for polish (2) was carried out to the front face of the base layer (1) which consists of a nonwoven fabric by the order above-mentioned [this invention] While said base layer (1) is formed in the double

laminated structure by the 1st base layer (1a) located in a surface layer (2) side, and the 2nd base layer (1b) of the rear face Said 1st base layer (1a) is JIS. It is specified to the degree of hardness of 80 degrees or more in the spring hardness test C form shown in K6301. Said 2nd base layer (1b) is JIS. Since it is characterized by what is specified to the degree of hardness of less than 80 degrees in the spring hardness test C form shown in K6301, respectively Without being influenced of the parallelism of a surface plate, or the thickness of a glue line, compression deformation of the abrasive cloth at the time of polish processing can be lessened, as a result end-face sagging of the polish article edge section can be controlled. And a surface layer not having a possibility of making a ground workpiece generating a fall, a blemish, etc. of surface roughness with the conventional thing since it is unchanging, and maintaining the good nature of a surface polish condition, it can control end-face sagging of the edge section, and can offer the polish workpiece of high quality.

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CLAIMS

[Claim(s)]

[Claim 1] In the abrasive cloth with which the laminating of the surface layer for polish (2) was carried out to the front face of the base layer (1) which consists of a nonwoven fabric While said base layer (1) is formed in the double laminated structure by the 1st base layer (1a) located in a surface layer (2) side, and the 2nd base layer (1b) of the rear face Said 1st base layer (1a) is JIS. It is specified to the degree of hardness of 80 degrees or more in the spring hardness test C form shown in K6301. Said 2nd base layer (1b) is JIS. Abrasive cloth characterized by what is specified to the degree of hardness of less than 80 degrees in the spring hardness test C form shown in K6301.

[Translation done.]

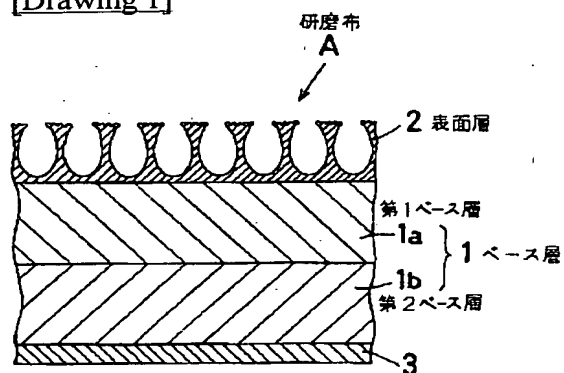
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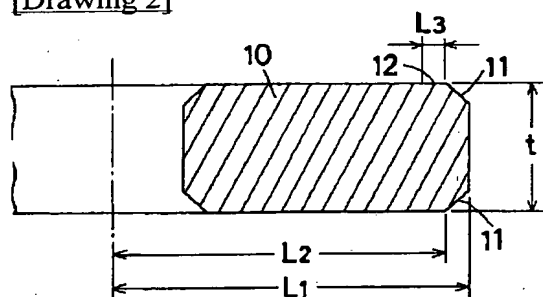
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DRAWINGS

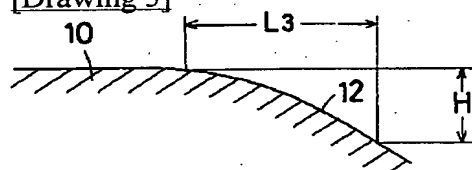
[Drawing 1]



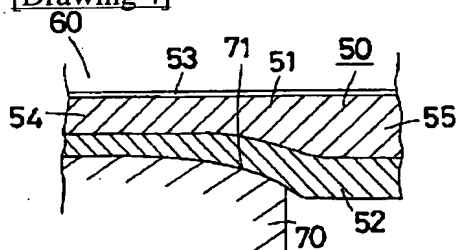
[Drawing 2]



[Drawing 3]



[Drawing 4]



[Translation done.]

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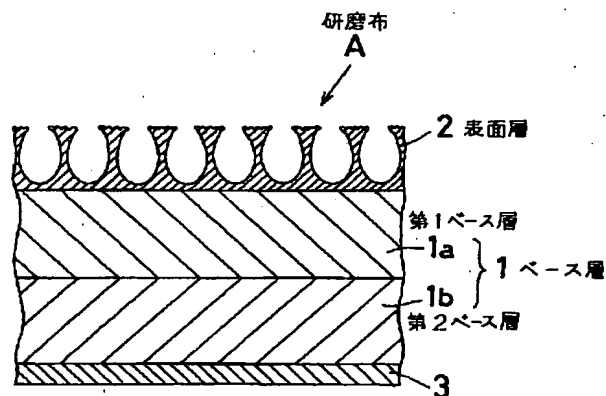
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(54) 【発明の名称】 研磨布

(57) 【要約】

【目的】 被研磨加工品について研磨加工時の表面粗度の低下や傷等の発生を招くことなく端面ダレを抑制し得る研磨布を提供する。

【構成】 不織布からなるベース層(1)の表面に研磨用表面層(2)が積層された研磨布を対象とする。そして、ベース層(1)が表面層(2)側に位置する第1ベース層(1a)とその裏面の第2ベース層(1b)とによる2重積層構造に形成されている。かつ第1ベース層(1a)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°以上に規定され、第2ベース層(1b)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°未満にそれぞれ規定されている。



【特許請求の範囲】

【請求項1】 不織布からなるベース層(1)の表面に研磨用表面層(2)が積層された研磨布において、前記ベース層(1)が表面層(2)側に位置する第1ベース層(1a)とその裏面の第2ベース層(1b)とによる2重積層構造に形成されるとともに、前記第1ベース層(1a)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°以上に規定され、前記第2ベース層(1b)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°未満に規定されていることを特徴とする研磨布。

【発明の詳細な説明】

【0001】

【産業上の利用分野】この発明はアルミニウム(その合金を含む)磁気ディスク基板、半導体用ウェハー、光学部品レンズ、ウェハー用マスク、金属サンプル等の研磨加工に用いられる研磨布に関する。

【0002】

【従来の技術】上記のような被研磨加工品の研磨加工は、例えば次のようにして行われる。即ち、水平式の両面研磨機の上下定盤に研磨布を接着した研磨機を用い、上下定盤を一定圧にて加圧して研磨布と被研磨加工品とを圧接する。そして、遊離砥粒を供給したのち、上下定盤及び被研磨加工品に回転運動を与え、研磨布と被研磨加工品とを摺動させることにより被研磨加工品の表面を研磨している。

【0003】上記例示したような研磨加工に用いられる研磨布は、一般に図4に示すように、ポリエステル繊維等の不織布からなるベース層(51)の表面にポリウレタン等からなる多孔質の研磨用表面層(52)が一体的に被覆形成され、さらにベース層(51)の裏面に定盤(60)への接着用の接着層(53)が被覆された構造を有している。

【0004】

【発明が解決しようとする課題】ところで、近時、被研磨加工品の小形、高精度化の要請に伴い、研磨加工についても加工後における厳しい表面特性が要求されるようになってきている。

【0005】しかるに、従来の研磨布を用いて研磨加工を行うと、図4に示すように、研磨布(50)の被研磨加工品(70)と接触する部分が弾力性により大きく圧縮変形される結果、変形部分(54)と非変形部分(55)との段差が大きくなり、このため変形部分(54)と非変形部分(55)との境界に位置する被研磨加工品(70)のエッジ部を湾曲状に覆って研磨布の表面が当接した状態となる。このような状態で研磨加工を行なうと、被研磨加工品(70)のエッジ部に斜め方向から大きな圧力が加わることから、エッジ部が傾斜状ないし円弧状に研磨されていわゆる端面ダレ(71)を生じるという問題があった。

【0006】このため、研磨布(50)の表面層(52)に硬化剤を含浸させることにより、研磨布の圧縮変形量を可及的に抑え、もって端面ダレを抑制する試みもなされてはいる。

【0007】しかし、この方法では硬化処理の程度が激しすぎると、被研磨加工品(70)の表面粗度の低下を招くとか、表面に傷やスクラッチ等を生じさせる原因となり、研磨加工後の良好な表面状態を得ることができないという新たな問題を派生するものであった。このため、表面層の硬化処理には限界があり、端面ダレの確実かつ十分な抑制を図ることができなかった。

【0008】また、ベース層(51)の厚さを薄くして研磨布全体の弾力性を抑え、もって圧縮変形量を少なくすることも試みられたが、ベース層(51)の厚さを薄くすると接着層(53)の厚さによる影響や、定盤(60)の傷、突起による影響が表面層(2)に承継され、やはり研磨加工後の表面特性に大きな影響を与えてしまうという問題を派生するものであった。

【0009】この発明は、かかる技術的背景に鑑みてなされたものであって、被研磨加工品について研磨加工時の表面粗度の低下や傷等の発生を招くことなく端面ダレを抑制し得る研磨布の提供を目的とする。

【0010】

【課題を解決するための手段】上記目的を達成するために、この発明は、図1の符号を参照して示すと、不織布からなるベース層(1)の表面に研磨用表面層(2)が積層された研磨布において、前記ベース層(1)が表面層(2)側に位置する第1ベース層(1a)とその裏面の第2ベース層(1b)とによる2重積層構造に形成されるとともに、前記第1ベース層(1a)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°以上に規定され、前記第2ベース層(1b)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°未満にそれぞれ規定されていることを特徴とする研磨布を要旨とするものである。

【0011】

【作用】表面層(2)に隣接する第1ベース層(1a)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°以上に規定されているから、第1ベース層(1a)ひいては研磨布全体の弾力性が低減され、研磨加工時に被研磨加工品に圧接したときの圧縮変形量が小さくなり、変形部分と非変形部分との段差が小さくなる。このため、研磨布の変形部分と非変形部分との境界に位置する被研磨加工品のエッジ部に付与される研磨布からの押圧力が軽減され、結果的に端面ダレが抑制される。一方、第2ベース層(1b)が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°未満に規定されているから、弾力性の低下による定盤平行度の影響が軽減され、研磨布の片すべりや研磨布の寿命短縮、さらには被研磨加工品の平行度異常

が防止される。

【0012】

【実施例】次に、この発明の実施例を説明する。

【0013】図1はこの発明の一実施例に係る研磨布 (A) を示すものである。図1において、(1) はポリエステル繊維製の不織布からなるベース層、(2) は該ベース層 (1) の表面に一体的に被覆形成されたポリウレタン製の研磨用表面層であり、該表面層 (2) は研磨加工に際して供給される遊離砥粒を保持すべく多孔質に形成されている。また、ベース層 (1) の裏面はプライマー処理されると共に、該裏面に両面テープからなる接着層 (3) が形成されており、この接着層 (3) を介して研磨布 (A) を定盤に接着し得るものとなされている。

【0014】また、この発明では、前記ベース層 (1) は第1ベース層 (1a) と第2ベース層 (1b) との二重積層構造をなすとともに、表面層 (2) に隣接する第1ベース層 (1a) が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°以上に規定され、第1ベース層 (1a) 裏面の第2ベース層 (1b) が、JIS K6301に示されたスプリングかたさ試験C形における硬度80°未満にそれぞれ規定された硬度を有するものとなされなければならない。JIS K6301に規定されたスプリングかたさ試験C形とは、試験片として原則として厚さ6mm以上のもの (6mm未満のものは積み重ねてなるべく6mm以上とする) を用い、この試験片をスプリングかたさ試験機のC形を用いて行う硬度測定試験であり、本来的には加硫ゴムのかたさを測定するための試験であるが、この発明ではこれを第1、第2ベース層 (1a) (1b) のかたさ試験として準用する。ここに、第1ベース層 (1a) の硬さが上記試験における硬度80°以上に規定されるのは、硬度80°未満では端面ダレの抑制を十分に図り得ないからである。即ち、硬度80°未満では第1ベース層が柔軟すぎて研磨加工時に被研磨加工品に圧接したときの圧縮変形量が大きすぎる結果、変形部分と非変形部分との段差が大きくなる。このため、研磨布の変形部分と非変形部分との境界に位置する被研磨加工品のエッジ部の全体に斜め方向からの大きな押圧力が付与され、結果的に端面ダレの発生を抑制し得ないからである。逆に言えば、第1ベー

ス層 (1a) を硬度80°以上とすることによって、研磨布の圧縮変形部分と非変形部分との変形量の差を少なくすることができ、エッジ部に付与される研磨布からの押圧力を軽減しえ、結果的に端面ダレの発生を抑制し得るからである。特に好ましくは、第1ベース層 (1a) の硬さはこれを上記試験における硬度90°以上に設定するのが良い。

【0015】ベース層 (1) を硬度80°以上に規定するための手段は特に限定されることはなく、例えば、ベース層を硬質の不織布で形成するとか、不織布の密度を増大するとか、軟質ベース層に硬化剤を含浸させるとかの方法を挙げ得る。

【0016】而して、第1ベース層 (1a) の硬さを上記に規定したことにより、第1ベース層 (1a) ひいては研磨布 (A) 全体の弾力性が低下し、このため定盤平行度の影響を受けやすくなって研磨布の片すべりの原因や、研磨布の寿命短縮、さらには被研磨加工品の平行度異常の原因となる。そこで、第2ベース層 (1b) の硬さをJIS K6301に示されたスプリングかたさ試験C形における硬度80°未満に規定することによりある程度の弾力性を確保し、上記不具合を防止するものである。

【0017】ちなみに、第1ベース層 (1a) の厚さ1.0mm、第2ベース層 (1b) の厚さ0.5mm、表面層 (2) の厚さ0.5mmに設定すると共に、第1ベース層 (1a)、第2ベース層 (1b) の硬度のみを、JIS K6301に規定されたスプリングかたさ試験C形においてそれぞれ下記表のように規定した数種類の研磨布を用い、端面ダレの発生状況を調べた。また、ベース層が1層構造である従来の研磨布を用いても同様の試験を行った。

【0018】なお、試験片として図2に示すように、直径L1:95mm、外側チャンファー部 (11) を除いた直径L2:94.7mm、厚さt:1.27mmのアルミニウム磁気ディスク基板 (10) を用い、外側チャンファー部 (11) の内側端縁から内方L3:4mmの範囲にわたってダレ測定部 (12) を設定し、このダレ測定部 (12) における端部の高低差H (図3に示す) をダレ量として測定した。その結果を表1に示す。

【0019】

【表1】

	第1ベース層硬度	第2ベース層硬度	ダレ量 (H) (μm)
従来例	なし	75°	0.3
比較例	75°	75°	0.25
実施例1	80°	75°	0.15
実施例2	90°	75°	0.08

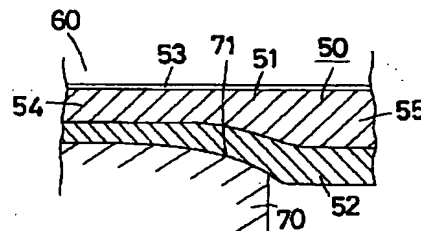
【0020】上記表1からわかるように、第1ベース層 (1a)、第2ベース層 (1b) の硬度を、本発明範囲に規定することにより、被研磨加工品の端面ダレを大幅に抑

制し得ることを確認し得た。

【0021】

【発明の効果】この発明は上述の次第で、不織布からな

2…表面層



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